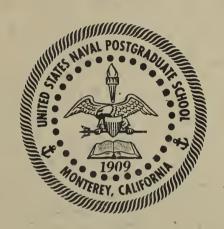
## UNITED STATES NAVAL POSTGRADUATE SCHOOL



# A DETAILED INTEGRATION FOR THE RADIATION IMPEDANCE OF A RHOMBIC ANTENNA

---BY---

CLARENCE FREDERICK KLAMM JR.

ASSISTANT PROFESSOR OF ELECTRONICS

A REPORT

TO THE NAVY DEPARTMENT
BUREAU OF SHIPS

UPON AN INVESTIGATION CONDUCTED UNDER BUSHIPS PROJECT ORDER NO. 10731/52

JUNE 1, 1952

TECHNICAL REPORT NO. 5

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#### A DETAILED INTEGRATION FOR THE RADIATION IMPEDANCE OF A RHOMBIC ANTENNA

Clarence F. Klamm Jr.
United States Naval Postgraduate School
Monterey, California

#### ABSTRACT

The generalized circuit equation derived by Chaney (1) is applied directly to evaluation of the radiation impedance of a terminated rhombic antenna in free space. The fact that certain integrations totalize to zero, as demonstrated by Chaney (2) from his equations of constraint, is verified by actual detailed evaluation of the integrals involved.

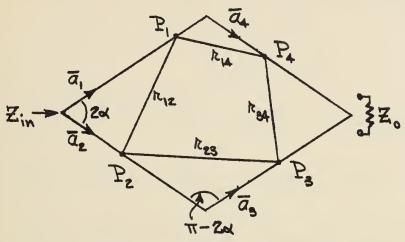
Furthermore, Chaney's formulae (2) for the radiation impedances of both the terminated rhombic and vee in free space are verified by independent integration.

<sup>1.</sup> J. G. Chaney, "A critical study of the circuit concept", J. Appl. Phys. 22, 12, 1429 (1951).

<sup>2.</sup> J. G. Chaney, "Free space radiation impedance of rhombic antenna", U. S. Naval Postgraduate School Technical Report No. 4 (BuShips Project Report No. 1) (May 1952).



# RADIATION IMPEDANCE OF THE TERMINATED RHOMBIC IN FREE SPACE



$$\overline{a}_1 = \overline{a}_3$$
 \  $\overline{a}_1 \cdot \overline{a}_1 = \overline{a}_2 \cdot \overline{a}_2 = 1$ 
 $\overline{a}_2 = \overline{a}_4$  \  $\overline{a}_1 \cdot \overline{a}_2 = 0$  and  $2$  and

$$\bar{I}_1 = \bar{a}_1 \bar{I}_0 e^{-i k x_1}$$
  
 $\bar{I}_2 = -\bar{a}_2 \bar{I}_0 e^{-i k x_2}$ 

$$\bar{I}_8 = -\bar{\alpha}_1 I_0 e^{-\frac{i}{2}k(l+x_0)}$$

$$\bar{I}_4 = \bar{\alpha}_2 \bar{I}_0 e^{-\frac{i}{2}k(l+x_0)}$$

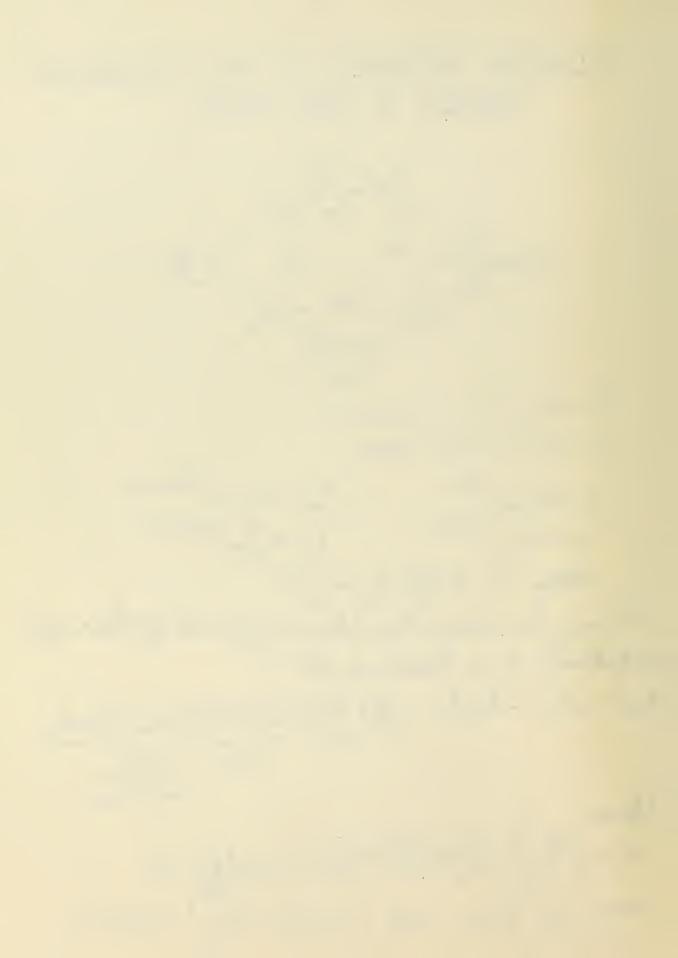
where I = length of any leg.

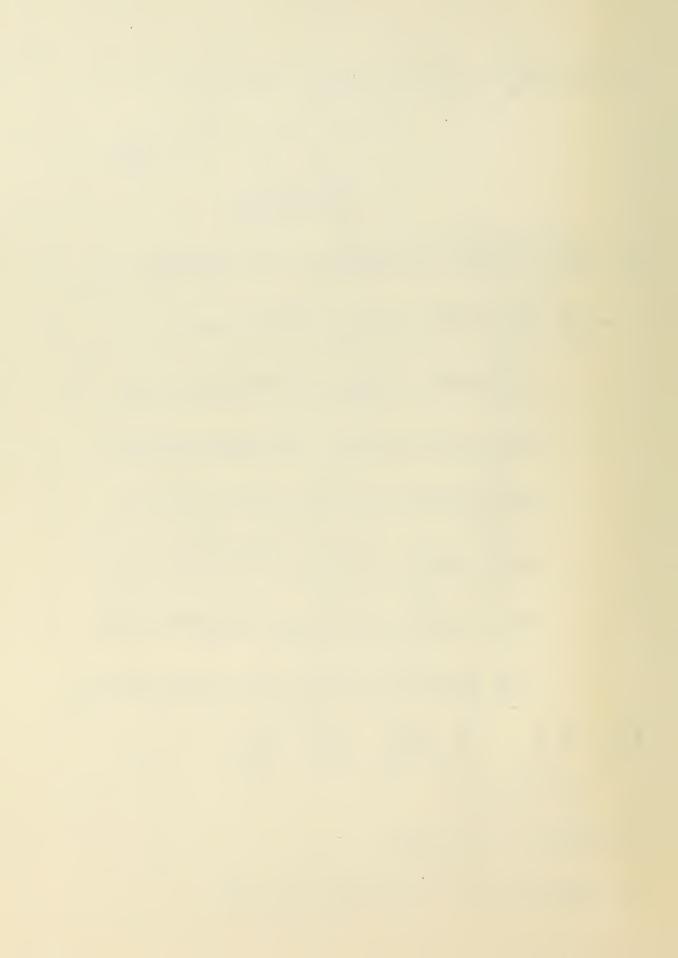
Chancy has derived the following formula for the input impedance of a closed circuit (1)

Zin - Zifil + 41 Zifi + 32 f f Pe [f(P)) f(P)] Q[e(R) dE] - dEe

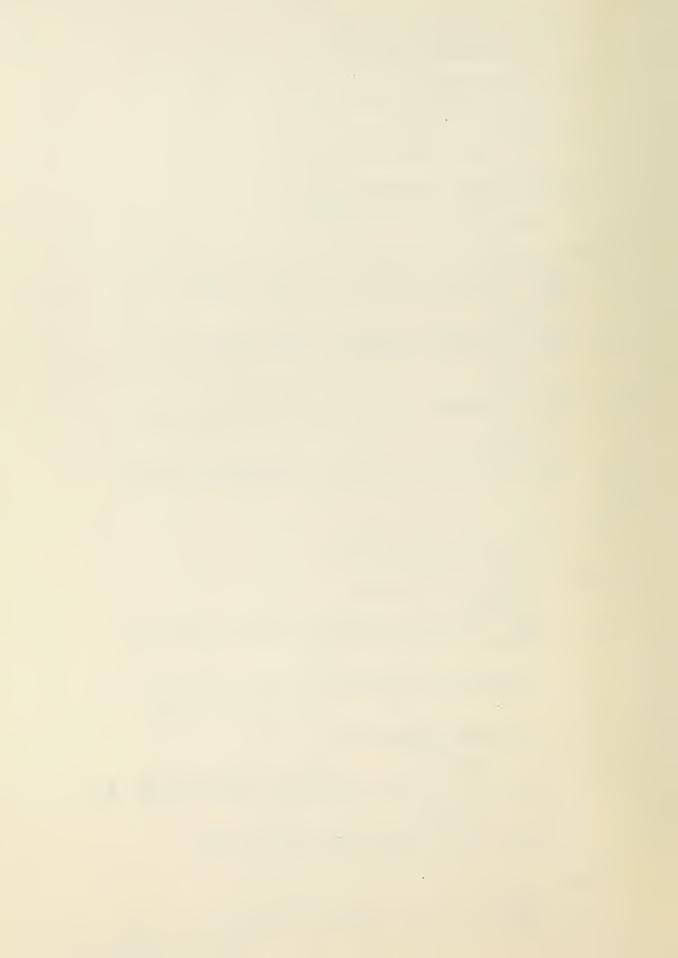
= Zr = radiation impedance

Thus,  $Z_{R} = \frac{30}{30} \sum_{i,j=1}^{4} f_{i} f$ 





$$\begin{aligned} & R_{23} = \sqrt{\alpha^2 + (x_3 - x_1 + \lambda_{000} \otimes 2)^2 + (\lambda_{000} \otimes 2)^2} \\ & R_{24} = \sqrt{\alpha^2 + (\lambda_1 - x_2)^2 + x_2^2 + 2(\lambda_1 - x_1) x_0 \omega_0 Z_{2d}} \\ & R_{14} = \sqrt{\alpha^2 + (\lambda_1 - x_2)^2 + x_2^2 + 2(\lambda_1 - x_1) x_0 \omega_0 Z_{2d}} \\ & R_{25} = \sqrt{\alpha^2 + (\lambda_1 - x_2)^2 + x_3^2 + 2(\lambda_1 - x_2) x_3 \omega_0 Z_{2d}} \\ & Deline; \\ & Z_{11} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 \omega_0 Z_0 + 2(\lambda_{12}) dx_1 dx_2 \\ & Z_{12} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_3 - \lambda_1) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 \omega_0 Z_0 + 2(\lambda_{12}) dx_1 dx_2 \\ & Z_{14} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_3 - \lambda_1) \frac{\delta^2}{\delta x_1 \delta x_3} - k^2 \omega_0 Z_0 + 2(\lambda_{12}) dx_1 dx_4 \\ & Z_{14} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_3 - \lambda_1) \frac{\delta^2}{\delta x_1 \delta x_3} - k^2 \omega_0 Z_0 + 2(\lambda_{12}) dx_1 dx_4 \\ & Z_{15} = 4(Z_{11} - Z_{12} - Z_{13} + Z_{14}) \\ & Z_{16} = 4(Z_{11} - Z_{12} - Z_{13} + Z_{14}) \\ & Z_{17} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{17} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 e(\lambda_{12}) dx_1 dx_2 \\ & Z_{18} = \frac{30}{30} \int_{0}^{\beta} \int_{0}^{\beta} \omega_0 k(x_1 - x_2) \frac{\delta^2}{\delta x_1 \delta x_2} - k^2 \omega_0 Z_0 + k(\lambda_$$

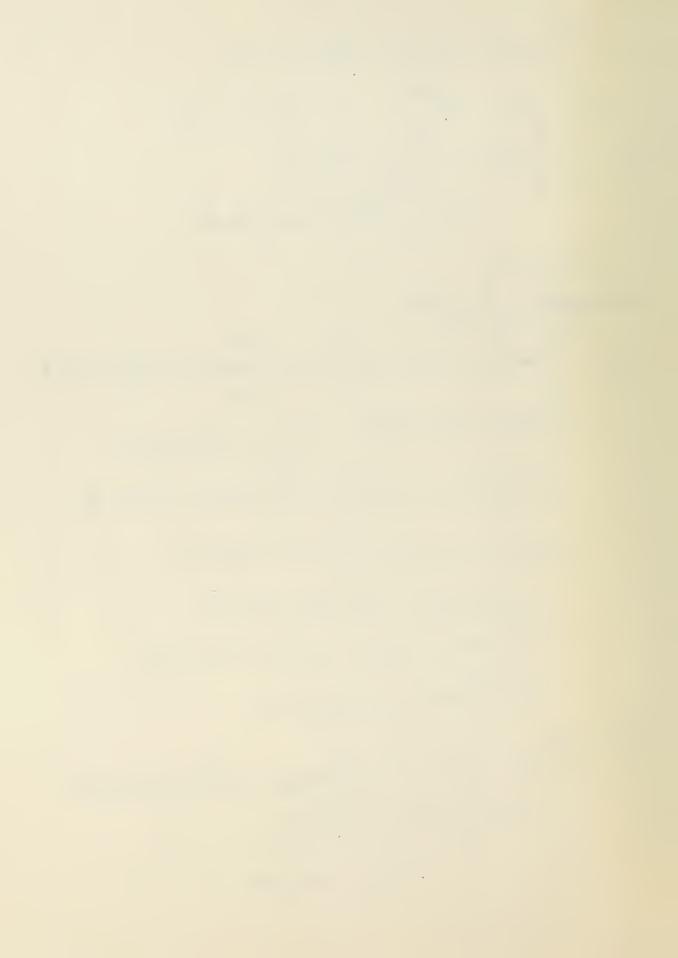


$$A_{11} = \int_{0}^{1} \int_{0}^{1} \cos k(x_{1} - x_{1}^{2}) \frac{e^{x}}{(2x_{1} - x_{1}^{2})} e(k_{11}) dx_{1} dx_{1}^{2}$$
where  $e(k_{11}) = \frac{e^{x} k k_{11}}{k_{11}}$ ,  $k_{11} = \sqrt{a^{2} + (x_{1} - x_{1}^{2})^{2}}$ 

$$A_{11} = \int_{0}^{1} \int_{0}^{1} \cos k(x_{1} - x_{1}^{2}) \frac{e^{x}}{2x_{1}^{2}} e(k_{11}) dx_{1} dx_{1}^{2}$$

$$- k_{2}^{2} \int_{0}^{1} \int_{0}^{1} \cos k(x_{1} - x_{1}^{2}) \frac{e^{x}}{2x_{1}^{2}} e(k_{11}) dx_{1}^{2} dx_{1}^{2}$$

$$= \int_{0}^{1} \cos k(x_{1} - x_{1}^{2}) \frac{e^{x}}{2x_{1}^{2}} e(k_{11}) dx_{1}^{2} dx_{1}^{$$



 $A_{11} = 2e(n_{20}) - 2\cos kl e(n_{20}) - 4k \int_{0}^{l} \sin kx_{1} e(n_{10}) dx_{1}$ 

Evaluate integral in last term

 $\int_{A}^{A} \ln k x_{1} e(k_{10}) dx_{1} = \int_{A}^{A} \frac{\ln k x_{1} \operatorname{cur} k x_{10}}{k_{10}} dx_{1} - \int_{A}^{A} \frac{\sinh k x_{10} \ln k x_{10}}{k_{10}} dx_{1}$   $= \frac{1}{2} \int_{A}^{A} \frac{\sinh k(k_{10} + \chi_{1})}{k_{10}} dx_{1} + \frac{1}{2} \int_{A}^{A} \frac{\sinh k(k_{10} - \chi_{1})}{k_{10}} dx_{1}$   $+ \frac{1}{2} \int_{A}^{A} \frac{\cosh k(k_{10} + \chi_{1})}{k_{10}} dx_{1} - \frac{1}{2} \int_{A}^{A} \frac{\cosh k(k_{10} - \chi_{1})}{k_{10}} dx_{1}$ 

The following well known integration formulae may be readily verified by the transformation  $u = k \pm Z$  (+or-as required).  $\int_{-\infty}^{\infty} \frac{1}{2} \left( \frac{1}{2} \left( \frac{1}{2} + \frac{1}{2} \right) - C(\beta(k_1 + Z_1)) \right) = 0$ where  $\int_{-\infty}^{\infty} \frac{1}{2} \left( \frac{1}{2} \left( \frac{1}{2} + \frac{1}{2} \right) - C(\beta(k_1 + Z_1)) \right) = 0$ where  $\int_{-\infty}^{\infty} \frac{1}{2} \left( \frac{1}{2} + \frac{1}{2} \right) dz = 0$ 

 $\int_{Z_{1}}^{Z_{2}} \beta(R+Z) dZ = Ci \beta(R_{2}+Z_{2}) - Ci \beta(R_{1}+Z_{1})$   $\int_{Z_{1}}^{Z_{2}} \beta(R+Z) dZ = Si \beta(R_{2}+Z_{2}) - Si \beta(R_{1}+Z_{1})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R+Z)}{R} dZ = Ci \beta(R_{1}-Z_{1}) - Ci \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Ci \beta(R_{1}-Z_{1}) - Ci \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$   $\int_{Z_{1}}^{Z_{2}} \frac{2i \beta(R-Z)}{R} dZ = Si \beta(R_{1}-Z_{1}) - Si \beta(R_{2}-Z_{2})$ 

 $\frac{1}{2} \left\{ \frac{\text{Sik}(R_{0}+1) - \text{Sika} - \text{Sik}(R_{0}-1) + \text{Sika}}{= \text{Si2kl}} + \frac{1}{3} \left[ \frac{\text{Cik}(R_{0}+1) - \text{Cika} + \text{Cik}(R_{0}-1) - \text{Cika}}{= \text{Cikl}} \right] - \frac{1}{2} \left\{ \frac{\text{Si2kl} + \frac{1}{3} \left[ \frac{\text{Cikl} - \text{Cika}}{2} + \frac{1}{3} \left[ \frac{\text{Cikl} - \text{Cikl}}{2} - \frac{\text{Cikl}}{2} + \frac{1}{3} \left[ \frac{\text{Cikl} - \text{Cikl}}{2} + \frac{1}{3} \left[ \frac{\text{Cikl}}{2} + \frac{1}{3$ 



Thus
$$A_{11} = \begin{bmatrix} z & -\frac{1+\cos 2kl}{2} - 2k \sin 2kl \end{bmatrix}$$

$$+ \delta \begin{bmatrix} -2k + \frac{\sin 2kl}{2} - 2k \cos 2kl + 2k \cos 2kl \end{bmatrix}$$

$$+ \delta \begin{bmatrix} -2k + \frac{\sin 2kl}{2} - 2k \cos 2kl + 2k \cos 2kl \end{bmatrix}$$

$$A_{12} = \int_{0}^{1} \int_{0}^{1} \cos k (x_{1} - x_{1}) (\frac{3^{2}}{2} - x_{1}^{2} + x_{2}^{2} - 2x_{1}^{2} \cos 2kl )$$

$$h_{12} = \sqrt{a^{2} + x_{1}^{2} + x_{2}^{2} - 2x_{1}^{2} \cos 2kl }$$

$$h_{12} = e(k_{10}) + e(k_{10}) - 2\cos kl e(k_{10}) - 2k \int_{0}^{1} \sin kx_{1} e(k_{10}) dx_{1}$$

$$- 2k \int_{0}^{1} \sin k(l - x_{1}) e(k_{11}) dx_{1}$$

$$= \frac{1}{2} \left\{ \sin k(l - x_{1}) e(k_{11}) dx_{1} - \frac{1}{2} \int_{0}^{1} \frac{\sin 2kx_{1}}{x_{1}} dx_{1} - \frac{1}{2} \int_{0}^{1} \frac{\cos 2kx_{1}}{x_{1}} dx_{1} \right\}$$

$$= \frac{1}{2} \left\{ \sin 2kx_{1} - \frac{1}{2} \int_{0}^{1} \frac{\sin 2kx_{1}}{x_{1}} dx_{1} - \frac{1}{2} \int_{0}^{1} \frac{\cos 2kx_{1}}{x_{1}} dx_{1} \right\}$$

$$= \frac{1}{2} \left\{ \sin 2kx_{1} - \frac{1}{2} \int_{0}^{1} \frac{\sin k(l - x_{1}) \cos kx_{1}}{x_{1}} dx_{1} - \frac{1}{2} \int_{0}^{1} \frac{\sin k(l - x_{1}) \cos kx_{1}}{x_{1}} dx_{1} \right\}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) \cos kx_{1}}{x_{1}} dx_{1} - \int_{0}^{1} \frac{\sin k(l - x_{1}) \cos kx_{1}}{x_{1}} dx_{1}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) \cos kx_{1}}{x_{1}} dx_{1} - \int_{0}^{1} \frac{\sin k(l - x_{1}) \cos kx_{1}}{x_{1}} dx_{1}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} dx_{1}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} dx_{1}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} dx_{1}$$

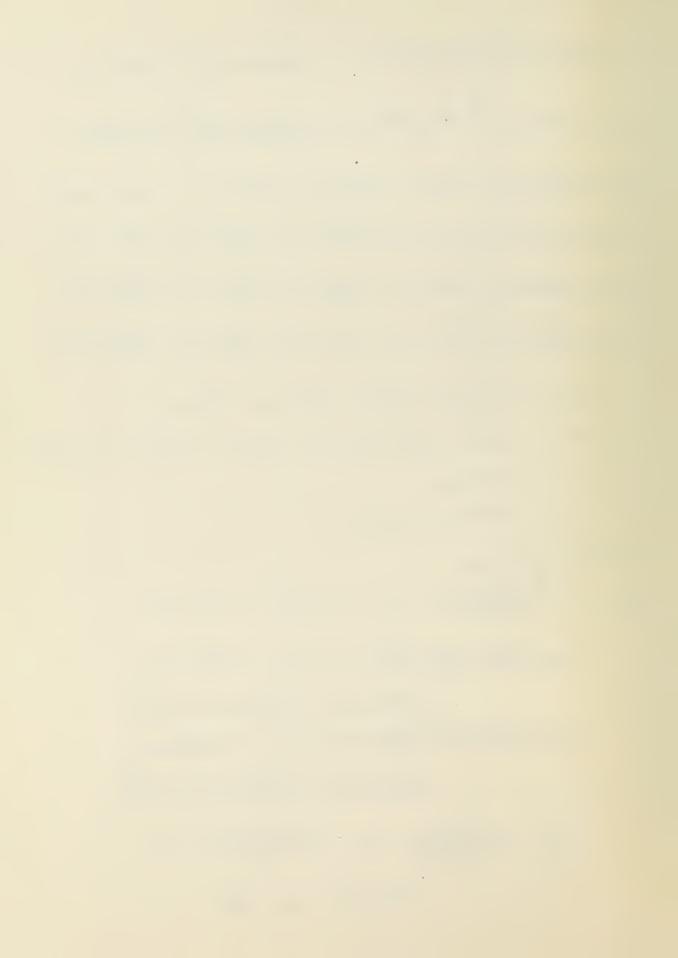
$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} dx_{1}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} - \int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} dx_{1}$$

$$\int_{0}^{1} \frac{\sin k(l - x_{1}) e(k_{11}) dx_{1}}{x_{1}} d$$



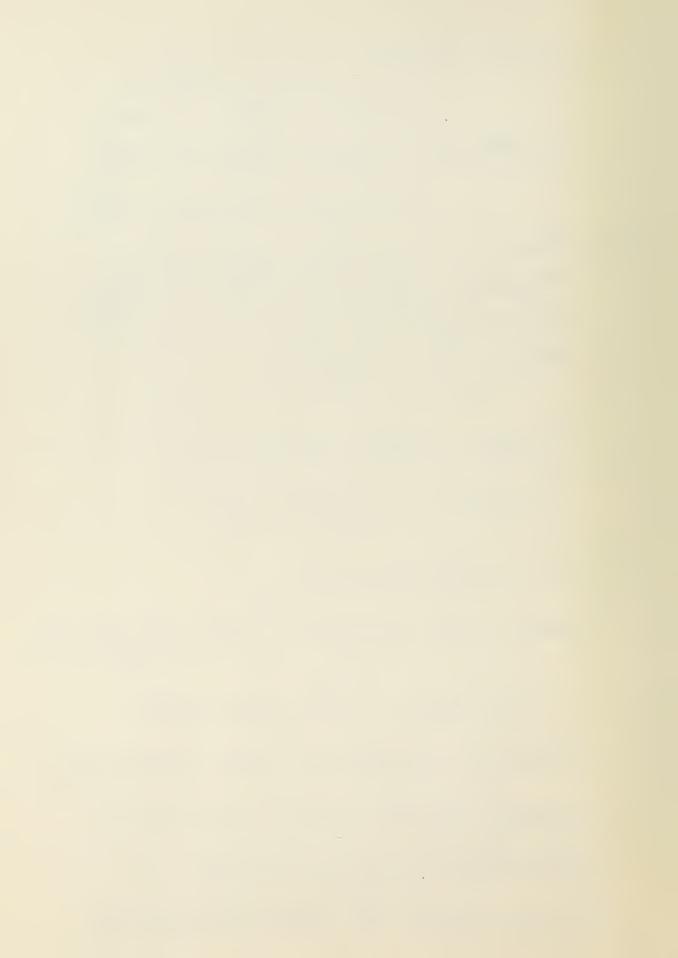
- join (Zhloinz) Jeoskx sinkx dx + jeos (Zkkinž) Jinkx sinkx dx =  $\frac{1}{2}$  sin(zklain2) [Cik(ke+x) - Cik(ke+x) + Cik(ke-x) - Cik(ke-x)]  $-\frac{1}{2}\cos(2klain2)\left[Sik(k_0+\chi_0)-Sik(k_0+\chi_0)-Sik(k_0-\chi_0)+Sik(k_0-\chi_0)\right]$ - = sin(2klain2) [Sik(ex+xx) - Sik(ex+xx) + Sik(ex-xx) - Sik(ex-xx)] + \frac{1}{2} cos(2) \land (2) \left (1/6-x) - (1/6 (1/6-x) - (1/6 (1/6-x) + (1/6 (1/6-x))) (Ro+xo= - 1204224+12in224-loss 24 = 21 sin2 /Rg+xg=-1/2(1-cox20)+/2xin22+2/ain2d=2/(sind+xin2d)  $k_0 - \chi_0 = 2 \log^2 \alpha$   $(\kappa_1 - \chi_1 = 2 (\text{sind-sin}^2 \alpha)$ Collecting terms-A12={ cos(2klains) + 1/a - 2 cos2kl - kSi2kl -kain(Zklain2)(Ci(Zklaina(1+aind)) - Ci(Zklain2) +Ci(2kless2)-Ci(2klaina(1-sind)]
+kcos(2klain2)[Si(2klaina(1+sind)) - Si(2klain2) -Si(Zkleosza) + Si(Zklaina (1-aira)) +if - sin (2klaine) - k + 2 sinklesskl + k C +kln2kl -kci2kl



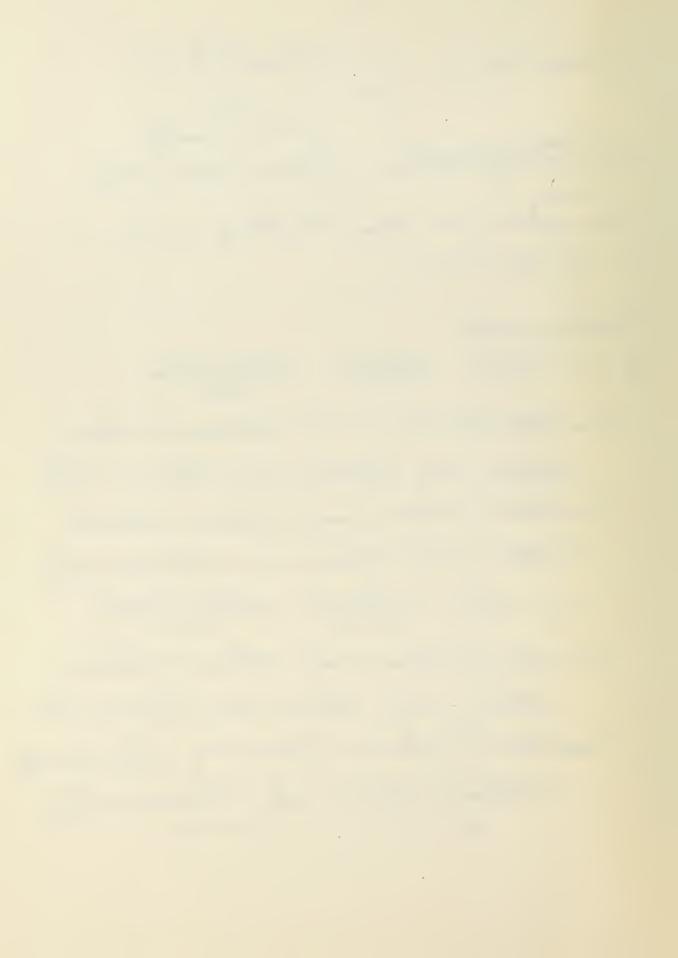
+ le sin(2klxin²2) Si(2klxinx(1+xind) - Si(2klxin²2)
+Si(2klcos²2) - Si(2klxinx(1-xind))
- le cos(2klxin²2) [Ci(2klcos²2) - Ci(2klxinx(1-xind))
+Ci(2klxin²2) - Ci(2klxinx(1+xind))
e: When  $\alpha = 0$ , reconsideration and the limits and

Note: When  $\alpha = 0$ , reconsideration of the limits of integration readily shows that  $A_{12}$  reduces to  $A_{11}$  as it should. This serves as a partial check on these integrations.

 $A_{13} = \int_{1}^{x} \int_{1}^{x} \cos k(x_{1} - x_{3} - k) \left( \frac{3^{2}}{3x_{1} 3x_{3}} - \frac{k^{2}}{2} \right) e(k_{13}) dx_{1} dx_{3}$  $R_{13} = \sqrt{\alpha^2 + (\chi_3 - \chi_1 + l\cos 2\alpha)^2 + (l\sin 2\alpha)^2}$ Coak(x,-x3-1) 22 (12) dx, dx3 = [ [ coa k(x,-x3-l) = 2(2,3) dx3+k] fink(x-x3-l)= e(2,3) dx, dx3 =  $\int_{0.04}^{0} k_{13} \frac{\partial}{\partial x_{3}} e(k_{13}) dx_{3} - \int_{0.04}^{0} k(x_{3}+1) \frac{\partial}{\partial x_{3}} e(k_{03}) dx_{3}$ + le [ [sink(x,-x3-1)e(r,3)]dx,+ le ] [cosk(x,-x3-1)e(r,3)dx,dx3 = cook x3e(k23) + & Sin &x3e(k23) dx3 - cook(x3+1) e(k03) -k faink(x3+1)e(203)dx3+ & faink(x-21)e(21)dx, - le Jaink(x,-1) e(c,0) dx, + le J J coa le (x,-x3-De(c,3) dx, dx3







$$A_{14} = \int_{0}^{l} \int_{0}^{l} \cos k(x_{1} - x_{4} - l) \left( \frac{3^{2}}{3x_{1}3x_{4}} - k^{2} \right) e(k_{14}) dx_{1} dx_{4}$$

$$R_{14} = \sqrt{\alpha^{2} + (l - x_{1})^{2} + x_{4}^{2} + 2(l - x_{1})x_{4} \cos 2\alpha}$$

Au = coskx elep/ + k frinkx elephdx - cosk(x+1)eleph)

-k frink(x+1)eleopdx + k frinkx, elephdx, - liphnkx, - lephkx, - lephkx

 $\begin{cases} k_{11} = 1 & k_{01} = 2 l \cos d \\ k_{10} = 2 & k_{00} = 1 \end{cases}$ 

 $A_{14} = coakl e(k_{1}) - e(k_{1}) - coa 2kl e(k_{0}) + coakl e(k_{0}) + 2k \int_{0}^{1} \sin k x_{4} e(k_{14}) dx_{4} - 2k \int_{0}^{1} \sin k (x_{4}+1) e(k_{0}+1) dx_{4}$ 

2 Sainkx+e(ce+)dx+ } kx=x+

(as in A12) = Sizkl-j[C+lnzkl-Cizkl]

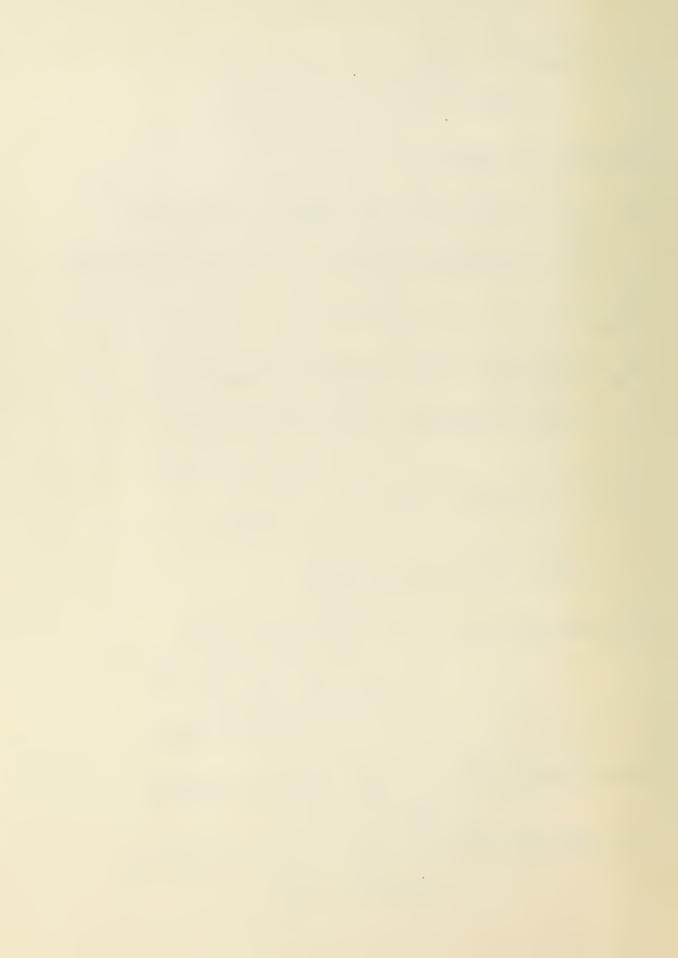
2 Saink(x4+1) e(x04) dx4 } R04 = 1/2+x2+2/x4042d

 $|x_{1}|^{2} = \sqrt{(x_{1}+(x_{2}+2)^{2}+2(x_{1}+x_{2}+2)^{2}+2(x_{1}+x_{2})^{2}}$   $|x_{2}|^{2} + |x_{2}|^{2} + |x_{1}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{1}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{1}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{2}|^{2} + |x_{1}|^{2} + |x_{2}|^{2} + |x_{$ 

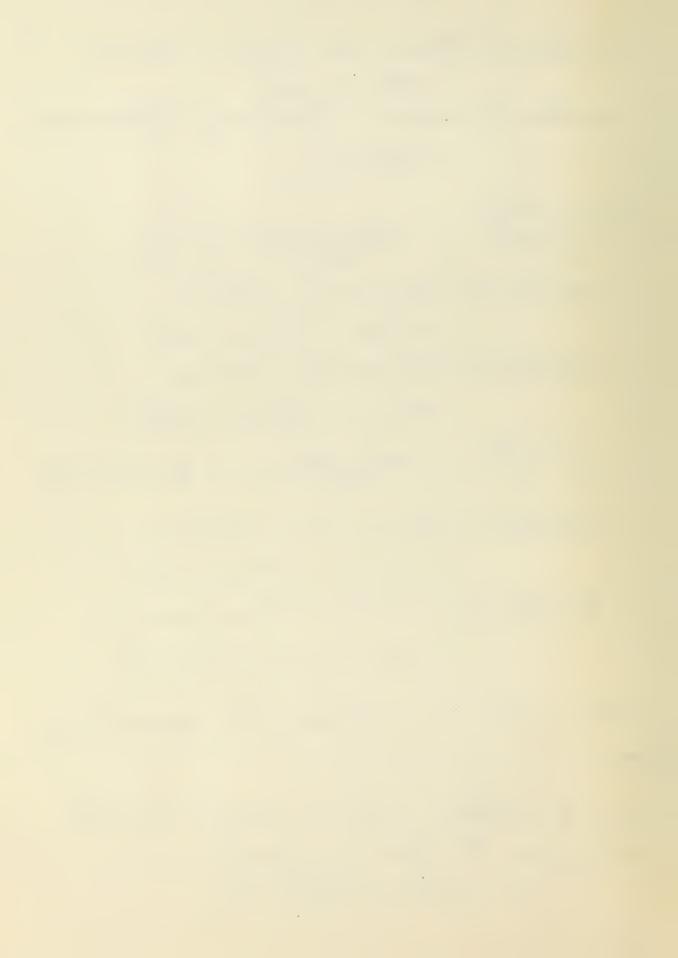
(as in A13)

= Ain (Zklain2) [Ci(Zklassell+essel) - Ci(Zklassel) + Ci(Zklain2)

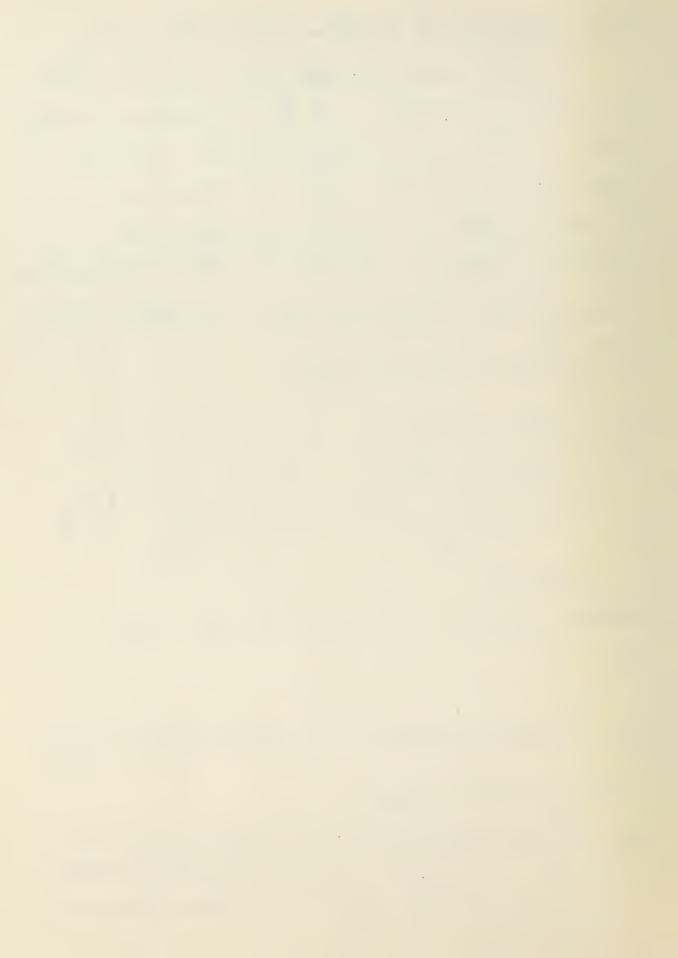
+ con(2klin3) [Si(2kl cood(1-cood)) - Si(2klcool) - Si(2klcool) - Si(2klcool) - Si(2klcool)



-jain(Zhlain2) Si(Zhlasa(1+cosa)) - Si(Zhlasa2) + Si(Zhlain2) -5 coa (2klain2) [Ci (2klain2) - Ci (2klasa(1-coa)) - Ci (2klasa(1+coa)) + (((Zklcod2)) Collecting results—  $A_{14} = \left\{ \frac{1 + \cos 2kl}{l} - \frac{1}{a} - \frac{\cos 2kl \cos(2kl \cos 2)}{2l \cos 2} + k Si 2kl \right\}$ -kain(2klain2)/(i/2klasa(1+cosa) - (i(2klasa2) + (i(2klain2) - (i(2klcodd(1-codd)) -kens (2klain2) [Si(2klased (1+cord)) - Si(2klase2) -Si(Rhlain2) + Si(Rhlcoad(1-coad)) +if- sin 2kl + k + cos 2kl sin (2klesse) - kl-kln 2kl + kli 2kl + kain (2klain 2) [Si(2kloodd(1+00d)) - Si(2kloodd) +Si(2klain2) - Si(2klood(1-coad)) +kcos (2klain2) [Ci(2klain2) - Ci(2klased (1-cosa)) - Ci(Zklessa (1+cosa) + Ci(Zklessa)) Adding up the above integrations with appropriate signs gives  $A_{11}-A_{12}-A_{13}+A_{14}=0$ hence the radiation impedance may be computed simply from the following expression, Zx = j 240 k min 2 (B12-B14),



which corresponds to Equation (22) of Chaney (2). Bizand Bix are evaluated below by the method described by Murray (3), and for comparison Murray's notation has been essentially retained. He has furthermore shown that unless the two linear integration paths lie in the same plane the impedance integrals will lead to untabulated functions. Therefore, B12 and B14 have been evaluated by taking all paths in the same plane.  $B_{12} = \int_{0}^{R} \int_{0}^{L} \frac{1}{2} \int_{0}^{R} \frac{1}{2} \int_{0}^{R}$  $= \frac{1}{2}(G_1 + G_1')$ Interchanging +, and + 2 gives G, = G', hence  $B_{12} = G_1$   $B_{14} = \int_0^1 \exp k(x_1 - x_4 - 1) e(x_{14}) dx_1 dx_4 \left\{ x_{14} - \frac{1}{2} (1 - x_1)^2 + x_4^2 + 2(1 - x_1) x_4 \cos 2x \right\}$ Letting x' = l-x, gives B<sub>H</sub> = \( \int\_{\cos} \( \text{R}(\text{X}\_1 + \text{X}\_4) \) \( (\text{R}\_{\text{A}}) \) \( \text{A}\_1 \) \( \text{A}\_2 \) \( \text{A}\_1 \) \( \text{A}\_1 \) \( \text{A}\_2 \) \( \text{A}\_1 \) \( \text{A}\_1 \) \( \text{A}\_1 \) \( \text{A}\_2 \) \( \text{A}\_1 \) \



Now the radiation impedance may be expressed  $Z_R = \frac{1}{5}120$  k sin  $\frac{2}{5}(2G_1 - G_2 - G_3)$ 

Evaluation of G:

 $G_1 = \int_0^1 \int_0^1 \frac{e^{i \frac{1}{k} (x_1 - x_2 - \kappa_{12})}}{\kappa_{12}} dx_1 dx_2$ 

$$|x_{12}| = \sqrt{x_1^2 + x_2^2 - 2x_1 x_2 \cos 2x}$$

$$= \sqrt{d_1^2 + (x_2 - cx_1)^2}$$

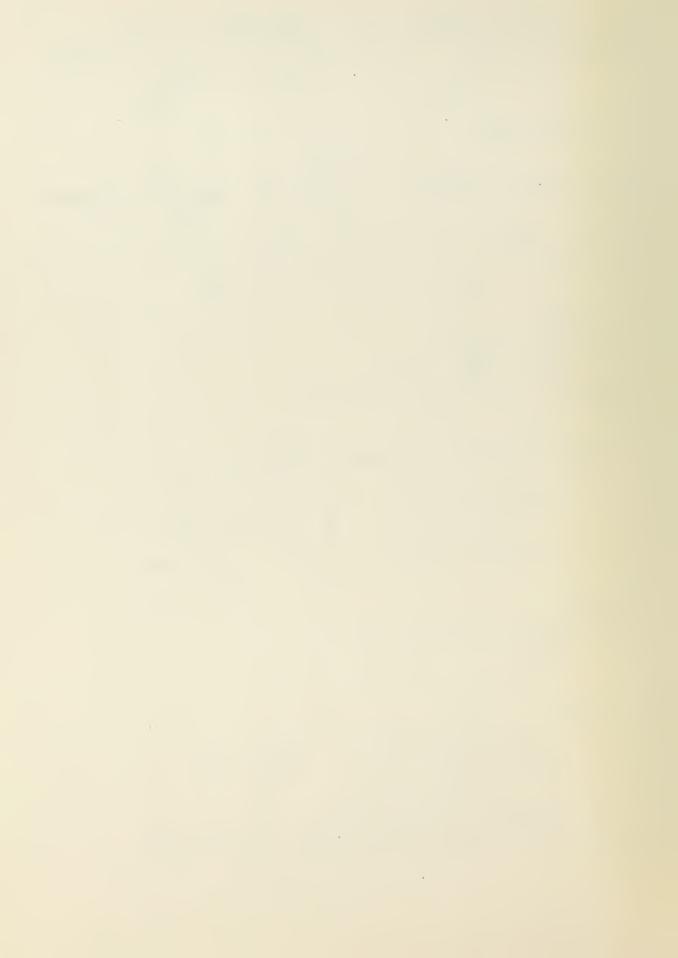
$$= \sqrt{d_1^2 + (x_1 - cx_2)^2}$$

$$= \sqrt{d_2^2 + (x_1 - cx_2)^2}$$

Let  $\begin{cases} d_1 t = k_{12} + (x_2 - ex_1) \\ d_1 t = k_{12} - (x_2 - ex_1) \end{cases}$ 

Then  $k_{12} = \frac{d_1}{2}(t + \frac{1}{2})$   $7z^{-2}x_1 = \frac{d_1}{2}(t - \frac{1}{2})$   $3x_2 = \frac{k_{12}}{2}$ 

G, = Sehxidx, Seh(x,+k,2) drz & h= jh



$$= \int_{0}^{R} e^{h(1-c)x} dx, \int_{t_{0}}^{t_{0}} \frac{e^{-hd_{1}t}}{t} dt = \int_{0}^{R} h(1-c)x dx, \int_{0}^{R} \frac{e^{-hd_{1}t}}{t} du$$

$$= \frac{1}{h(1-c)} \left\{ e^{h(1-c)x}, \int_{0}^{t_{0}} \frac{e^{-hd_{1}t}}{t} du \right\} - \int_{0}^{R} h(1-c)x \left[ e^{-hd_{1}t} \frac{h(1-c)}{h(1-c)} dt \right] dx$$

$$= \frac{1}{h(1-c)} \left\{ F(R) - F(O) - [J_{R} - J_{O}] \right\}$$

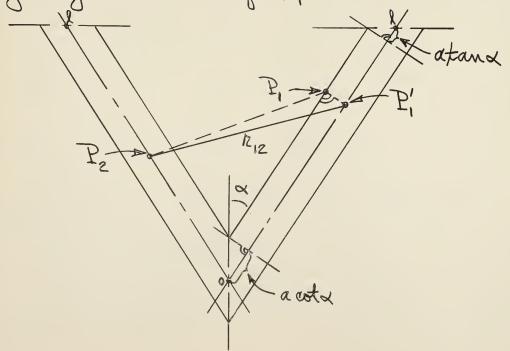
$$= \frac{1}{h(1-c)} \left\{ F(R) - F(O) - [J_{R} - J_{O}] \right\}$$

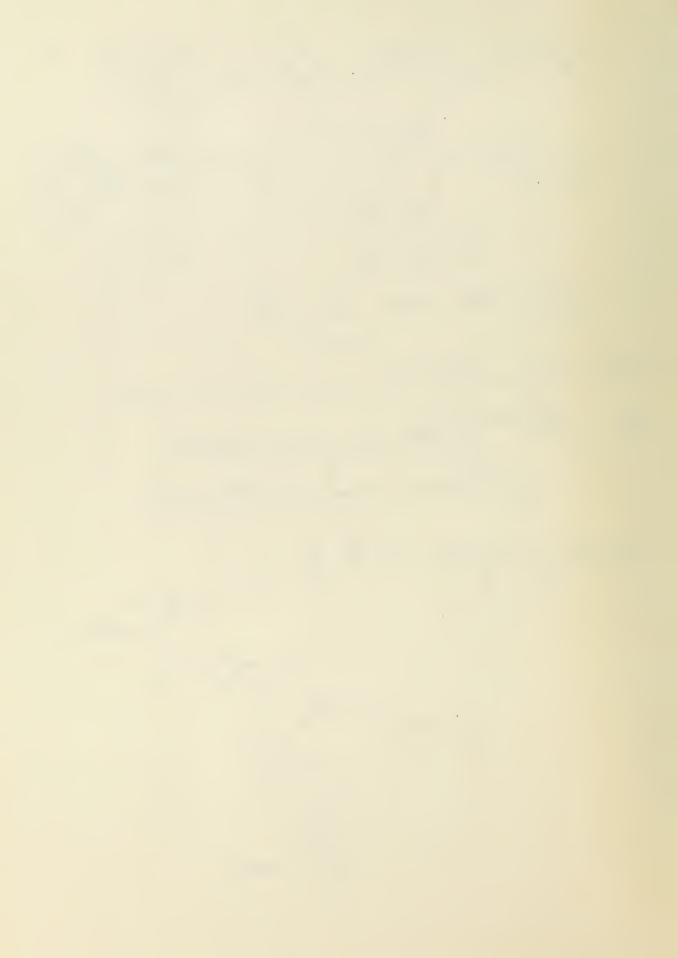
 $\left[ R_{1} + (l - ex_{1}) \right]_{\ell} = l - \left[ R(1 - e) + l(1 - e) \right] = Rlain \times (1 + ain x)$ 

F(1) = ¿Zklaina [Ci(zklaina (1+Aina)) - Ci(zklaina)

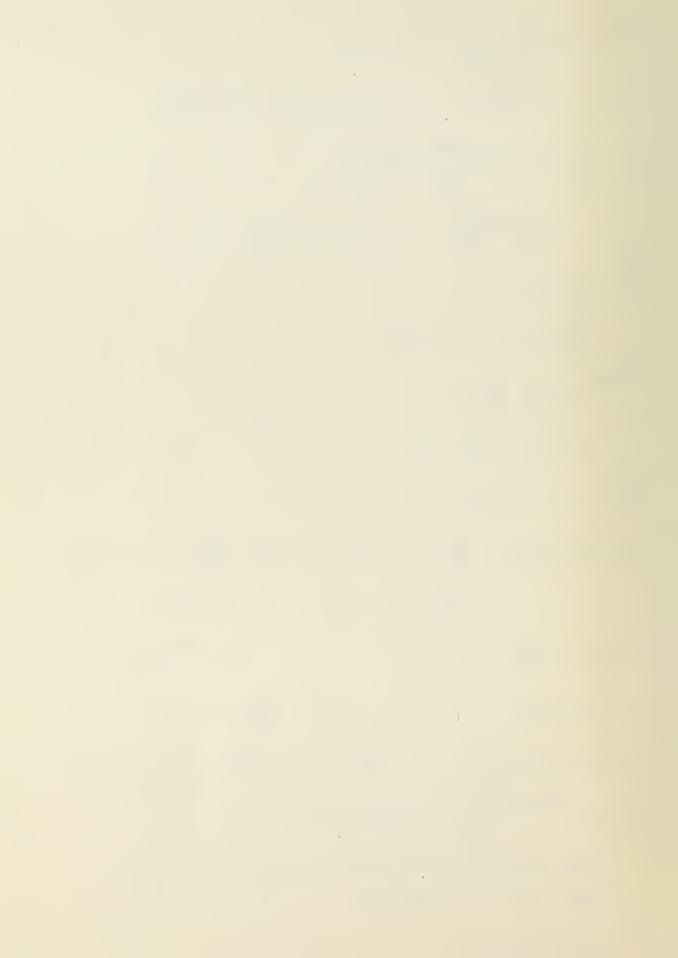
-j Si(zklaina (1+Aina)) + j Si(zklaina)

Selecting integration limits for x:





Zkx, sin² ] a cota = ka sin 2d F(0) = Ci(2kl) - C-ln(ka sin 2d) - j Si(2kl)  $J_{i} = \int_{e}^{l} h(1-e)x_{i} \left[ \frac{e^{-hd_{i}t_{l}}}{d_{i}t_{0}} \frac{\partial(d_{i}t_{0})}{\partial x_{i}} \right] dx_{i}$  $\frac{1}{d_1 t_2} \frac{\partial (d_1 t_2)}{\partial x_1} = \frac{1}{R_{10} + (l - cx_1)} \left( \frac{\partial k_1}{\partial x_1} - c \right)$ Let  $\begin{cases} d_{1}u = k_{1}e^{-(x_{1}-c)} \\ d_{2}u = k_{1}e^{+(x_{1}-c)} \end{cases}$ Then  $k_{11} = \frac{d_1}{2}(u + \frac{1}{u})$  $\frac{2\pi}{2^{1/2}} = -\frac{1}{\sqrt{2}}$ x,-el = = (u-1)  $\frac{\partial k_{i}\ell}{\partial x_{i}} - c = \frac{\chi_{i} - c\ell - ck_{i}\ell}{k_{i}c}$  $x_1 - el - e \times_{12} = -\frac{de}{de} \left[ u - \frac{1}{u} + e(u + \frac{1}{u}) \right] = -\frac{de}{de} \left[ u(1 + e) - \frac{1}{u}(1 - e) \right]$  $= -\frac{d_{1}(1+c)}{2u} \left[ u^{2} - y^{2} \right]$   $= -\frac{d_{1}(1+c)}{2u} \left[ u^{2} - y^{2} \right]$   $= -\frac{d_{1}(1+c)}{2u} \left[ u^{2} - y^{2} \right]$   $= -\frac{d_{2}(1+c)}{2u} \left[ u^{2} - y^{2} \right]$ dri = du k, + (1-ex):  $c_{X,-}(1-s^2)l = -\frac{cd_2}{u}(u-\frac{1}{u})$  $R_{11}+1-cx_{1}=\frac{d_{2}}{2}[u+\frac{1}{u}+\frac{2s^{2}l}{d_{2}}+c(u-\frac{1}{u})]=\frac{d_{2}}{2u}(u+b)^{2}$  $J_{k} = e^{-h(1-c)k} \int_{1}^{u_{k}} \frac{e^{-hd_{k}u}(u-tand)}{u(u+tand)} du$ ¿ daux = k2x-l(1-0) = 2 laina(1-sina) {dxu0= l(1+c) = 2l cox2d



$$J_{1} = e^{-\frac{i}{2}klain^{2}} \left\{ -\int_{u_{0}}^{u_{2}} \frac{e^{-hd_{1}u}}{u} du + Z \int_{u_{0}}^{u_{2}} \frac{e^{-hd_{2}u}}{u} du^{2}} \right\}$$

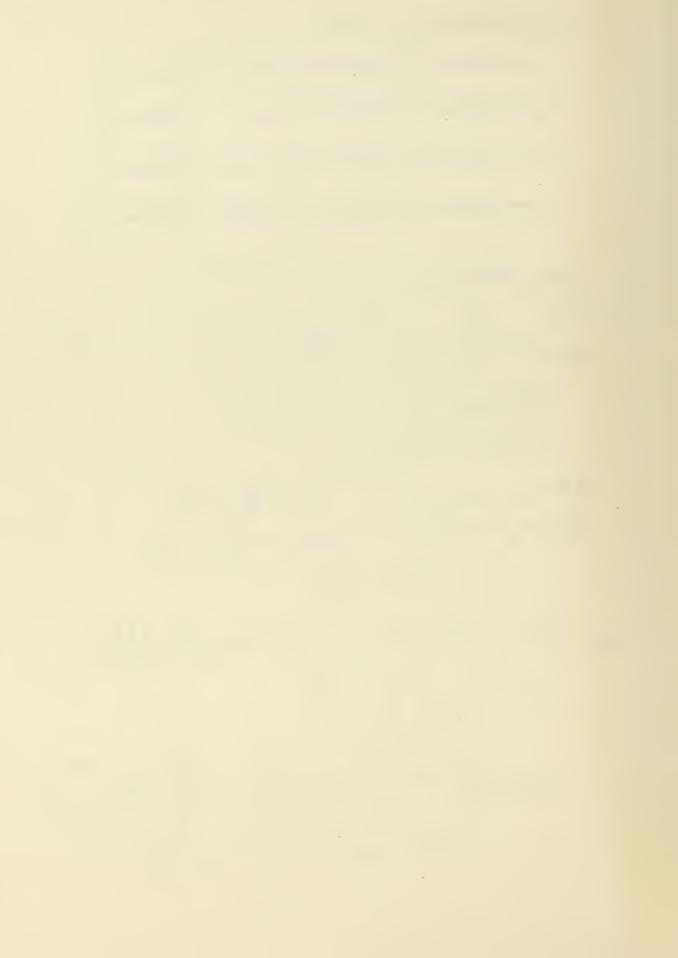
$$= e^{-\frac{i}{2}klain^{2}u} \left\{ -\int_{u_{0}}^{2klain_{1}u} \frac{du}{u} + 2e^{-\frac{i}{2}klain_{2}u} \frac{e^{-\frac{i}{2}u^{2}}}{u^{2}} du^{2}} \right\}$$

$$= e^{-\frac{i}{2}klain^{2}u} \left\{ -\int_{u_{0}}^{2klain_{1}u} \frac{du}{u} + 2e^{-\frac{i}{2}klain_{2}u} \frac{e^{-\frac{i}{2}u^{2}}}{u^{2}} du^{2}} \right\}$$

$$= e^{-\frac{i}{2}klain_{2}u} \left\{ \frac{e^{-\frac{i}{2}u^{2}}}{e^{-\frac{i}{2}u^{2}}} \frac{e^{-\frac{i}{2}u^{2}}}{u^{2}} \frac{e^{-\frac{i}{2}u^{2}}}{u^{2}}} \frac{e^{-\frac{i}{2}u^{2}}}{u^{2}} \frac{e^{-\frac{i}{2}u^{2}}}{$$



$$\begin{array}{l} +_{3}^{4} 2 Si(2kl \sin \lambda) -_{3}^{4} Si(2kl \cos \lambda) -_{3}^{4} Si(2kl \sin \lambda) -_{3}^{4} Si$$



$$F(l) = e^{\frac{i}{2}k(l-a)l} \left\{ \text{Cic}(2kl\cos u(l-\cos u)) - \text{Cic}(2kl\sin u) - \frac{i}{2}\text{Cic}(2kl\sin u) - \frac{i}{2}\text{Cic}(2kl\sin u) - \frac{i}{2}\text{Cic}(2kl\sin u) \right\}$$

$$k_{11} = 2l\cos u$$

$$k_{11} - (l+cx_{1}) = \sqrt{l^{2} + 2kl\tan \cos 2u + a^{2} \tan u} - (l+a\tan u\cos 2u)$$

$$= \frac{2a^{2}}{a} \sin u - \frac{2a}{a} \sin u - \frac{2a\sin u}{a\cos u}$$

$$F(0) = \frac{2a\sin u}{a\cos u} - \frac{2a\sin u}{a\cos u} - \frac{2a\sin u}{a\cos u}$$

$$J_{1} = \int_{0}^{1} e^{h(l-c)x_{1}} \left[ \frac{e^{-hd_{1}t_{1}}}{d_{1}t_{1}} \frac{3(d_{1}t_{2})}{3x_{1}} \right] dx_{1}$$

$$= \frac{1}{d_{1}t_{1}} \frac{3(d_{1}t_{2})}{3x_{1}} - \frac{1}{k_{1}u - (l+cx_{1})} (\frac{3k_{1}t_{2}}{3x_{1}} - c)$$

$$d_{1}u = k_{1}u - (x_{1} + cl) \qquad k_{1}u = \frac{d_{2}}{2}(u + \frac{1}{u})$$

$$\frac{3k_{1}u}{3u} - \frac{k_{1}u}{3u} - \frac{k_{1}u}{2}$$

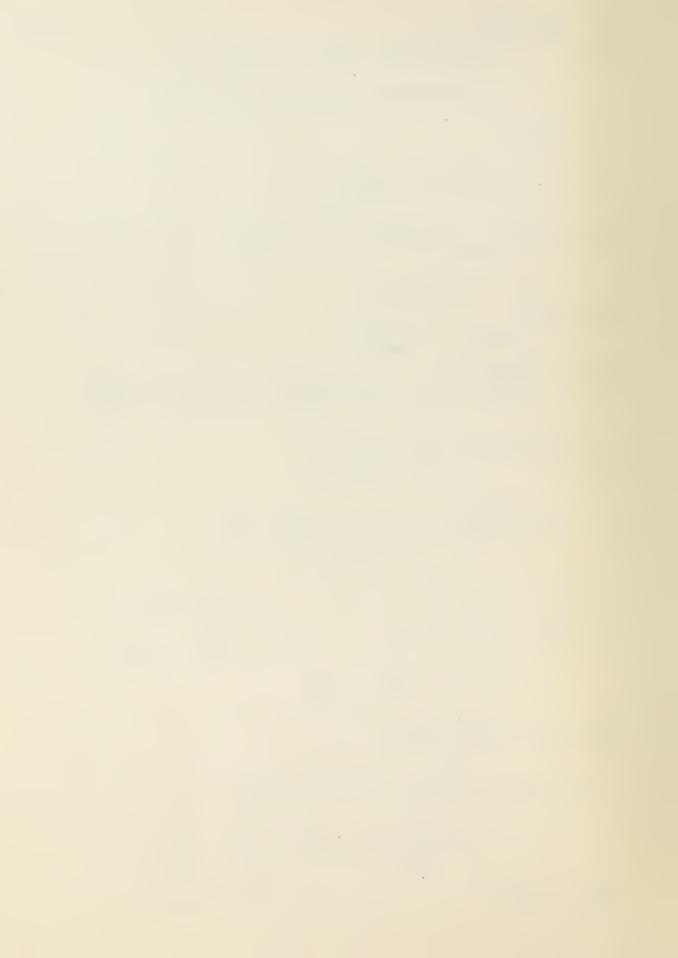
$$\frac{3k_{1}u}{3u} - c - \frac{x_{1}-cl-ck_{1}u}{2} \frac{k_{1}u}{2u} - \frac{1}{u} + c(u + \frac{1}{u})$$

$$= -\frac{d_{2}(1+c)}{2u} (u^{2} - v^{2})$$

$$\frac{3}{2} \frac{v^{2}}{1+c} - \frac{1-c}{1+c}$$

$$\frac{dx_{1}}{k_{1}u} - \frac{du}{u}$$

$$\frac{dx_{1}}{k_{1}u} - \frac{du}{u}$$



$$R_{11} = 1 - \alpha x_{1}; \qquad Cx_{1} + (1 - 3x) 1 = -\frac{d_{2}C}{2}(u - \frac{1}{u})$$

$$= \frac{d_{2}(1 + \alpha)}{2}(u - \frac{1}{2})^{2}$$

$$= \frac{d_{2}$$



$$G_{2} = -\frac{1}{32k \sin^{2}\alpha} \left\{ E(1) - E(0) - J_{1} + J_{0} \right\}$$

$$= -\frac{1}{32k \sin^{2}\alpha} \left\{ 2\ln(2k \ln 2) + 2C - 2C'(2k \ln 2 - 2n \ln 2) - 2\ln(2n \ln 2) \right\}$$

$$+ 2\cos(2k \ln 2) \left[ C'(2k \ln 2) - C'(2k \ln 2) - C'(2k \ln 2) \right]$$

$$+ 2\sin(2k \ln 2) \left[ C'(2k \ln 2) - C'(2k \ln 2) \right]$$

$$-\frac{1}{3} \cos(2k \ln 2) \left[ C'(2k \ln 2) - C'(2k \ln 2) \right]$$

$$-\frac{1}{3} \cos(2k \ln 2) \left[ C'(2k \ln 2) - C'(2k \ln 2) \right]$$

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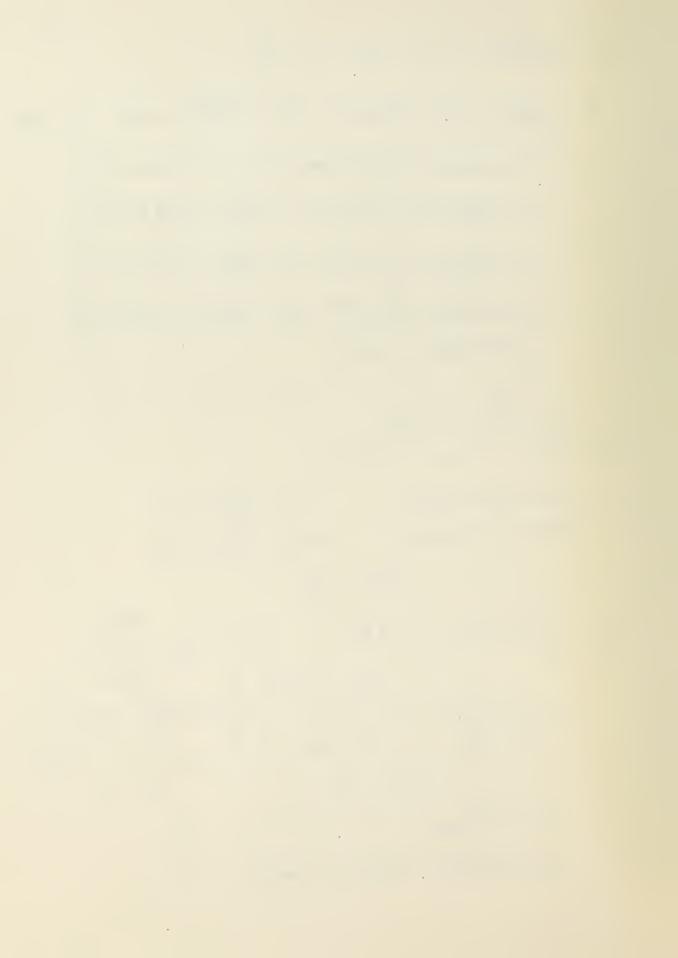
$$-\frac{1}{3} \cos(2k \ln 2) \left[ C'(2k \ln 2) \right]$$

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$$-\frac{1}{3} \cos(2k \ln 2) \left[ C'(2k \ln 2) \right]$$

R12+2(1+0) = 21 cos x (1+ cos x)



$$F(l) = e^{-\frac{i}{2}kl\sin^{2}x} \left\{ \frac{2i(2kl\cos x)(1+\cos x)}{2k(2kl\cos x)} - \frac{2i(2kl\cos x)}{2k(2kl\cos x)} - \frac{2i(2kl\cos x)}{2k(2kl\cos x)} \right\}$$

$$[k_{11}+(k+cx_{1})] = 2l$$

$$2kx_{1}\cos^{2}x = ka\sin^{2}x$$

$$E(0) = e^{-\frac{i}{2}(2kl)} - e^{-\frac{i}{2}(kx_{1})} \frac{3i(\frac{1}{2})}{3x_{1}} dx_{1}$$

$$\frac{1}{d_{1}t_{1}} \frac{3i(\frac{1}{2}t_{1})}{3x_{1}} = \frac{1}{k_{12}+(k+cx_{1})} \frac{3k_{12}}{3x_{1}} + e$$

$$\frac{1}{d_{1}t_{1}} \frac{3i(\frac{1}{2}t_{1})}{3x_{1}} = \frac{1}{k_{12}+(k+cx_{1})} \frac{3k_{12}}{3x_{1}} + e$$

$$\frac{1}{d_{1}t_{1}} \frac{3i(\frac{1}{2}t_{1})}{3x_{1}} = \frac{1}{k_{12}+(k+cx_{1})} \frac{3k_{12}}{3x_{1}} + e$$

$$\frac{3k_{12}}{3u} + k_{12} - (x_{1}+el) \qquad x_{1}+el = \frac{4i}{2}(u-\frac{1}{u})$$

$$\frac{3k_{12}}{3x_{1}} + e = \frac{4i}{2}[u-\frac{1}{u}+e(u+\frac{1}{u})]$$

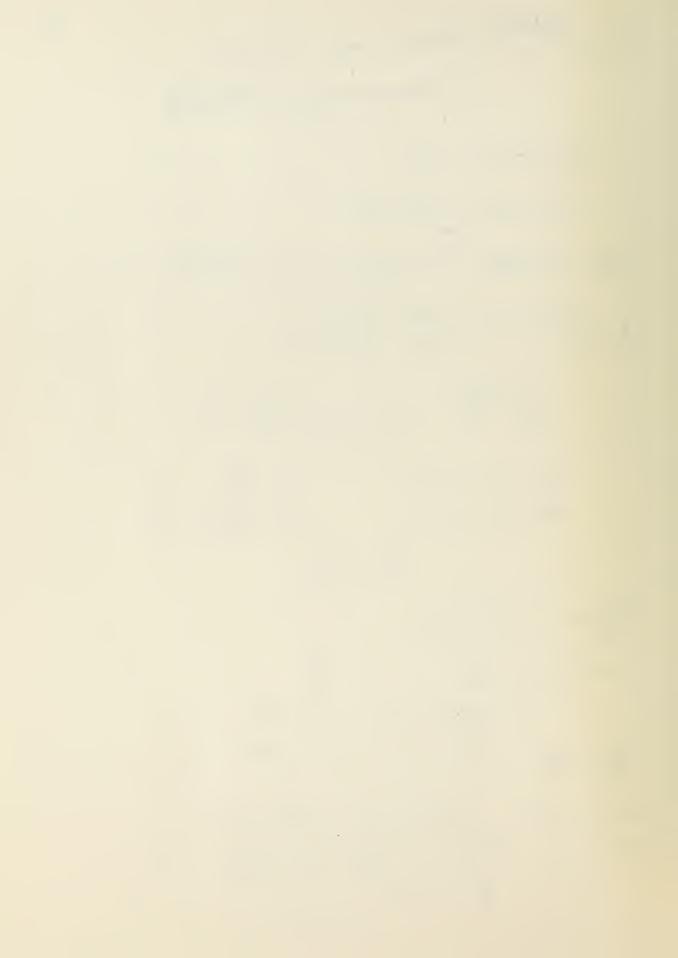
$$= \frac{4i(1+e)}{2u}(u^{2}-v^{2}) \stackrel{?}{>} v^{2} = \frac{1-e}{1+e}$$

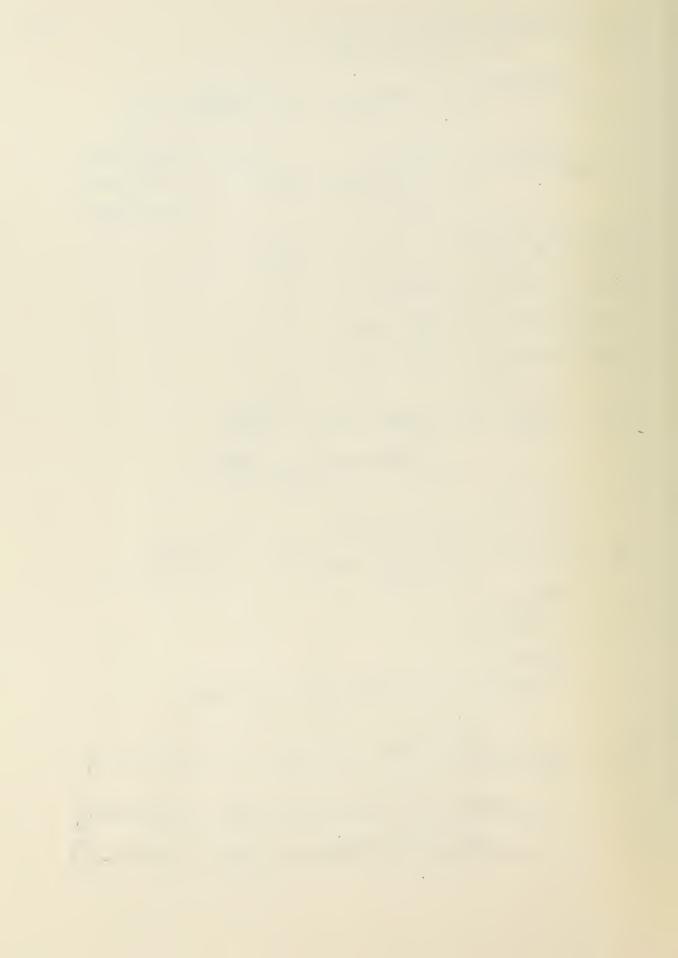
$$k_{12} + 4cx_{1} = \frac{4i}{2}[u-\frac{1}{u}+e(u+\frac{1}{u})]$$

$$= \frac{4i}{2u}(u+v)^{2}$$

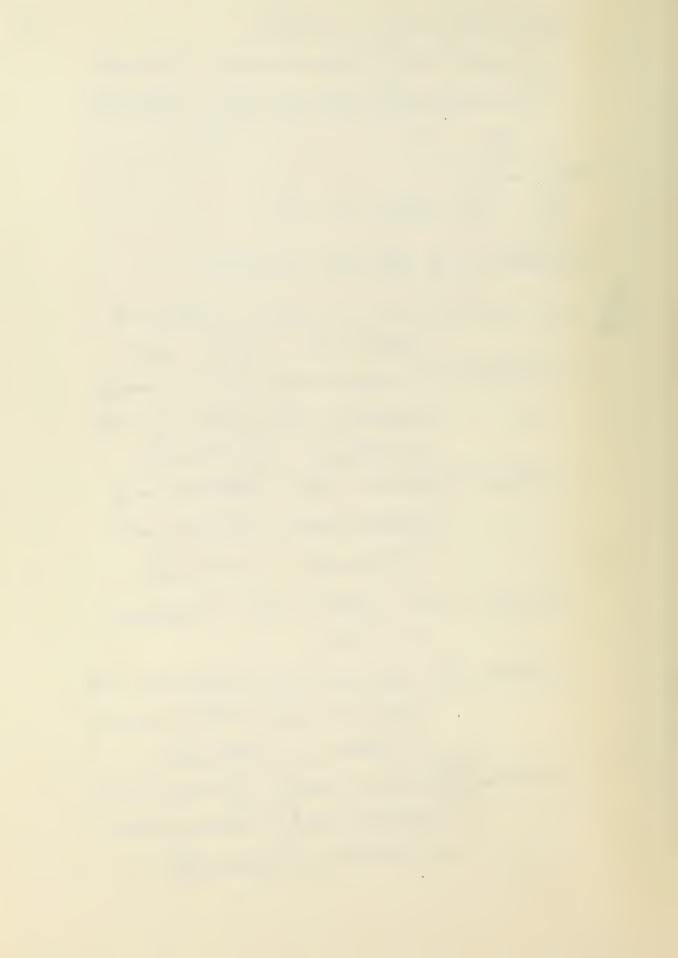
$$k_{12}+k_{12}+cx_{1} = \frac{4i}{2}[u+\frac{1}{u}+\frac{2s^{2}l}{4x}+e(u-\frac{1}{u})]$$

$$= \frac{4i}{2u}(u+v)^{2}$$





+;[25i(2kl(1+000))-25i(2kl)] - ¿2 cos(2klsin2) Si(2klcosd(1+cosd) - Si(2klcos2) -j2 sin(2klain2)[Ci(2klan2) - Ci(2klan2) Now from p. 15 120 = jk sin 2 (2G, -G2-G3) Substituting for the G's now gives 120 = 20 + 2ln(2klsin2d) + 20i(2kl) - 20i(2klsind) - Ci(2kl(1+cosa)) - Ci(2kl(1-cosa)) + coa(2klain2) (i(2klosa)(1-cosa)+(i(2klaina(1-aina)) + Ci(2klood(1+cod)+ Ci(2kloind(1+sing) - 2 Ci (2klros²) - 2 Ci (2klain²) + sin(2klain2)[Si/2klcosd(1-cosd) - Si/2klaind(1-sin3) -Sickland(1+com)+Sickland(1-mind) +251(2kloss2) - 251(2kloin2) + if Si(2kl(1+cos)) - Si(2kl(1-cos)) + 2Si(2klaind) -25i(2kl) + coa(2klain2) - Si(2kland(1-and) - Si(2klaind(1-aind)) -Si(2klassd(1+and))-Si(2klaind(1+sind) +25i(2klcod2)+25i(2klain2) + sin(2klain2) (c/2klased(1-cosa) - Ci/2klaine(1-sina) - Ci(2kl cood (1+cood) + Ci(2klaind(1+aind)) +2((2klcox22)-2(i(2klain22))}



## RADIATION IMPEDANCE OF THE TERMINATED VEE IN FREE SPACE

The radiation impedance of the see may be readily computed now from Chaney's formula for the input impedance of the closed pircuit \* except that now the open end of the vee is assumed closed through the terminating impedance. If the leg length is I and the vector angle 2x as before, and the same notation is employed as for the knowbic, the obvious result is obtained

$$Z_{R} = 2(Z_{11} - Z_{12})$$

$$= \frac{60}{3R}(A_{11} - A_{12} - 2R_{Ain}^{2} a B_{12})$$

$$\frac{Z_R}{60} = \frac{1}{i k} (A_{11} - A_{12}) + i 2k ain a G_1$$

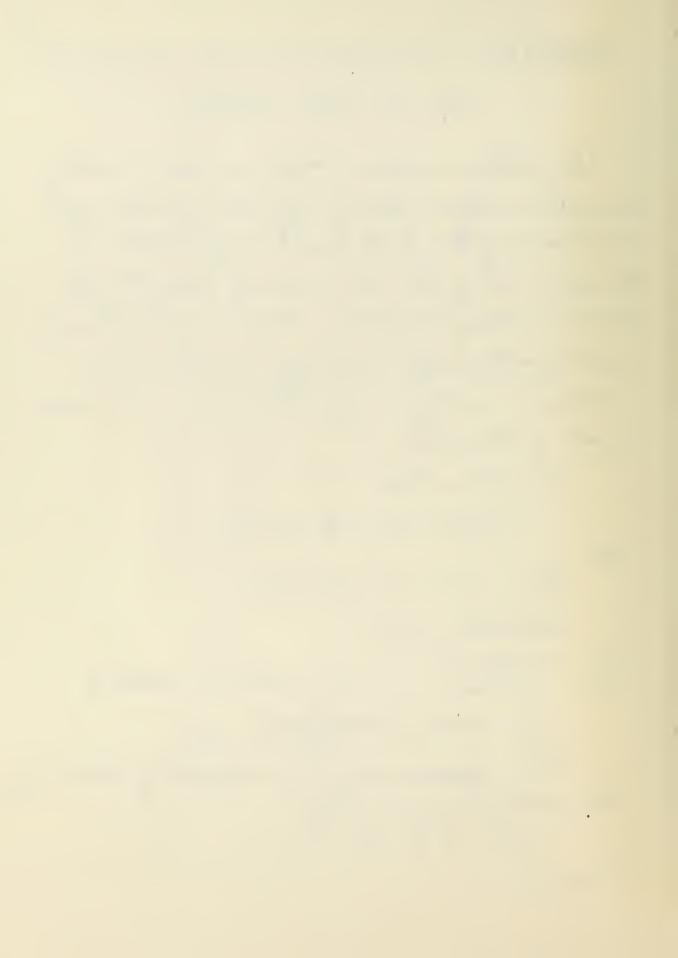
Substitution gives
$$\frac{Z_R}{60} = \frac{\text{sin}(2klaind)}{2klaind} - 1 + 2[C + \ln(2klaind) - Ci(2klaind)]$$

+ ¿[2 Si(Zklaina) + coa(Zklaina) - 1 | Ra]

This expression may be simplified by introducing the modified cosine integral

Cin x = C+ lmx - Cix

<sup>\*</sup> See p.2.

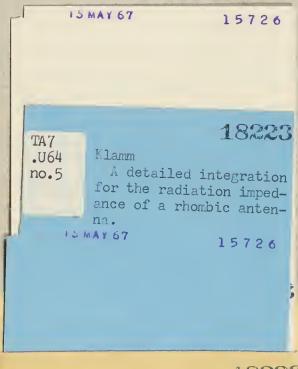


and by noting that the reactive components

represent the capacitance existing between the open ends of the nee. Since this capacitive reactance is shouted by the terminating impedance Z, these latter terms may be discarded as being negligible. Thus finally

\frac{Z\_R}{60} = \frac{\sin(2\klaina)}{2\klaina} - 1 + 2 \cin(2\klaina) + j 2 \si(2\klaina)





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